

Orchestrating on-board sensors for global hybrid robust stabilization of unicycles

Philipp Braun

School of Engineering,
Australian National University, Canberra, Australia

In Collaboration with:

- R. Ballaben: Faculty of Engineering, University of Porto (Portugal)
- A. Astolfi: Applied Mathematics and Computational Science, King Abdullah University of Science and Technology (Saudi Arabia)
- L. Zaccarian: Dipartimento di Ingegneria Industriale, University of Trento (Italy); and
Laboratoire d'Analyse et d'Architecture des Systèmes-Centre National de la Recherche Scientifique, Université de Toulouse, CNRS (France)



Australian
National
University

• Introduction and background

- Setting & Hybrid Systems & Lyapunov Stability

• Target stabilization

- Unmanned Ground Vehicles (UGV)

• Recent Extensions

- Unmanned Surface Vehicles (USV)

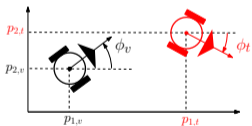
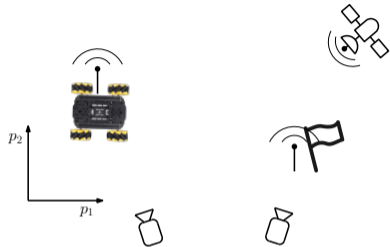


Ballaben, R., Astolfi, A., Braun, P., & Zaccarian, L. (2026b). *Orchestrating on-board sensors for global hybrid robust stabilization of unicycles* [Automatica]. <https://hal.science/hal-05004452>

What measurements can we use to close the loop?



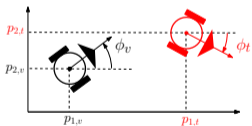
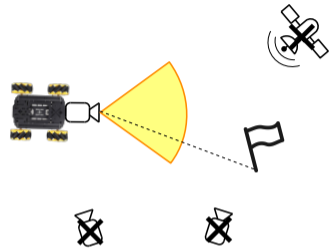
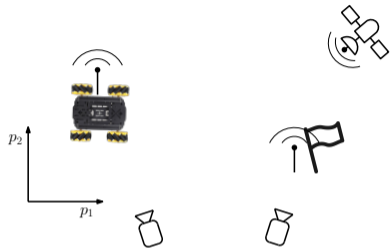
What measurements can we use to close the loop?



Cartesian coordinates

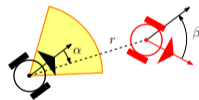
$$\begin{bmatrix} p_1 \\ p_2 \\ \phi \end{bmatrix} = \begin{bmatrix} p_{1,v} - p_{1,t} \\ p_{2,v} - p_{2,t} \\ \phi_v - \phi_t \end{bmatrix}$$

What measurements can we use to close the loop?



Cartesian coordinates

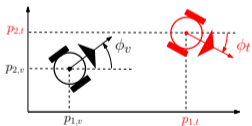
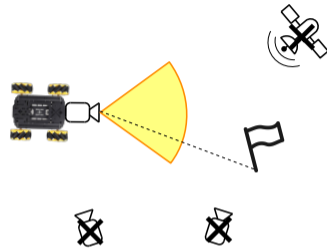
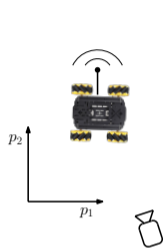
$$\begin{bmatrix} p_1 \\ p_2 \\ \phi \end{bmatrix} = \begin{bmatrix} p_{1,v} - p_{1,t} \\ p_{2,v} - p_{2,t} \\ \phi_v - \phi_t \end{bmatrix}$$



Camera-based coordinates

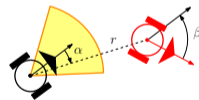
$$z = \begin{bmatrix} r \\ \beta \\ \alpha \end{bmatrix}, \quad \alpha \in [-\bar{\alpha}, \bar{\alpha}]$$

What measurements can we use to close the loop?



Coordinate transformation

$$\begin{bmatrix} p_1 \\ p_2 \\ \phi \end{bmatrix} = \gamma(z) := \begin{bmatrix} r \cos(\alpha - \beta - \pi) \\ r \sin(\alpha - \beta - \pi) \\ -\beta \end{bmatrix}$$



Cartesian coordinates

$$\begin{bmatrix} p_1 \\ p_2 \\ \phi \end{bmatrix} = \begin{bmatrix} p_{1,v} - p_{1,t} \\ p_{2,v} - p_{2,t} \\ \phi_v - \phi_t \end{bmatrix}$$

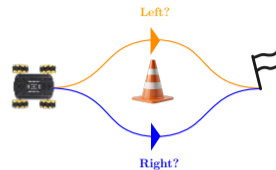
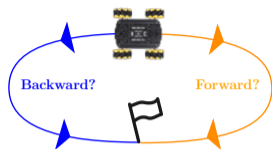
Stabilization using camera measurements

- If $(r, \alpha) \rightarrow 0$, then $(p_1, p_2) \rightarrow 0$
- Additionally, if $\beta \rightarrow 0$, then $\phi \rightarrow 0$

Camera-based coordinates

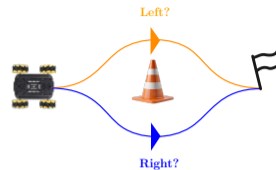
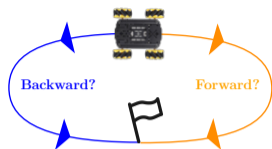
$$z = \begin{bmatrix} r \\ \beta \\ \alpha \end{bmatrix}, \quad \alpha \in [-\bar{\alpha}, \bar{\alpha}]$$

Decisions naturally arise when controlling a vehicle



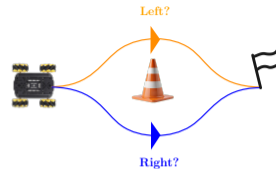
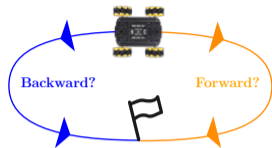
Decisions are discontinuous control actions...

Decisions naturally arise when controlling a vehicle



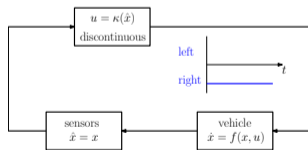
Decisions are discontinuous control actions... and they are necessary

Decisions naturally arise when controlling a vehicle

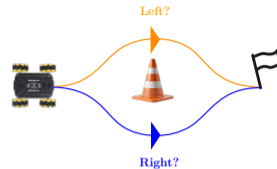
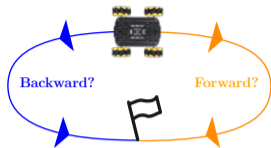


Decisions are discontinuous control actions... and they are necessary

- Discontinuous controllers work well in theory

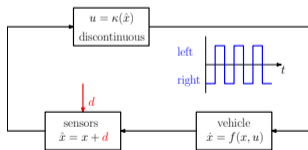


Decisions naturally arise when controlling a vehicle

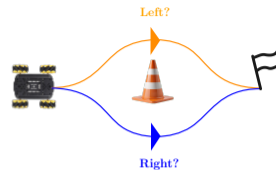
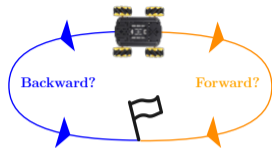


Decisions are discontinuous control actions... and they are necessary

- Discontinuous controllers work well in theory **but perturbations can be disruptive**

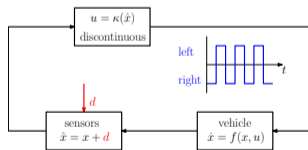


Decisions naturally arise when controlling a vehicle



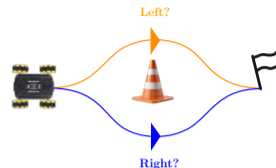
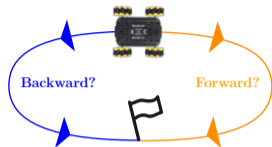
Decisions are discontinuous control actions... and they are necessary

- Discontinuous controllers work well in theory **but perturbations can be disruptive**



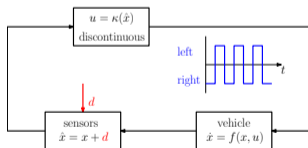
Discontinuous actions should be implemented in a **robust** way

Decisions naturally arise when controlling a vehicle



Decisions are discontinuous control actions... and they are necessary

- Discontinuous controllers work well in theory **but perturbations can be disruptive**



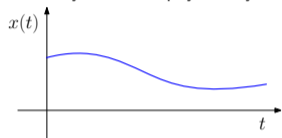
- Intrinsic limitations (Brockett, 1982)
 - Using path-planning with tracking (Pathak & Agrawal, 2005)
 - Discontinuous feedback (De Luca et al., 2000; Oelen et al., 1994) (σ -process coordinate change (Arnold, 1987))
 - Time-invariant sample-and-hold (Astolfi, 1996, 1998, 1999),
 - Discontinuous time-varying sample-and-hold (Braun et al., 2017; Pomet et al., 1992).
 - Uniting local+global (Prieur, 2001; Prieur & Astolfi, 2003)
 - Onboard sensors (Murrieri et al., 2004; Restrepo et al., 2021)
- Issues with angular winding

Discontinuous actions should be implemented in a **robust** way

Continuous-time systems

$$\dot{x} = f(x), \quad x \in \mathbb{R}^n$$

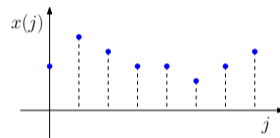
Model the dynamics of physical systems



Discrete-time systems

$$x^+ = g(x), \quad x \in \mathbb{R}^n$$

Model instantaneous events

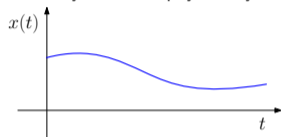


Hybrid dynamical systems [Teel, Goebel, Sanfelice, 2012]: a tool for modeling discont. actions

Continuous-time systems

$$\dot{x} = f(x), \quad x \in \mathbb{R}^n$$

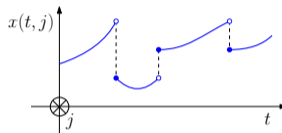
Model the dynamics of physical systems



Hybrid dynamical systems

$$\begin{cases} \dot{x} = f(x), & x \in \mathcal{C}, \\ x^+ = g(x), & x \in \mathcal{D}. \end{cases}$$

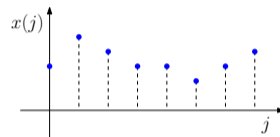
Combine both worlds



Discrete-time systems

$$x^+ = g(x), \quad x \in \mathbb{R}^n$$

Model instantaneous events



Hybrid dynamical systems [Teel, Goebel, Sanfelice, 2012]: a tool for modeling discont. actions

Continuous-time systems

$$\dot{x} = f(x), \quad x \in \mathbb{R}^n$$

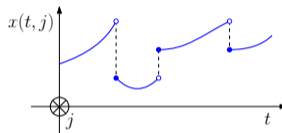
Model the dynamics of physical systems



Hybrid dynamical systems

$$\begin{cases} \dot{x} = f(x), & x \in \mathcal{C}, \\ x^+ = g(x), & x \in \mathcal{D}. \end{cases}$$

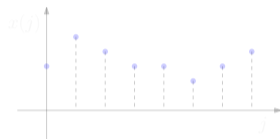
Combine both worlds



Discrete-time systems

$$x^+ = g(x), \quad x \in \mathbb{R}^n$$

Model instantaneous events



Terminology:

- f flow map
- \mathcal{C} flow set
- g jump map
- \mathcal{D} jump set

Continuous-time systems

$$\dot{x} = f(x), \quad x \in \mathbb{R}^n$$

Model the dynamics of physical systems



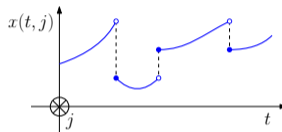
Terminology:

- f flow map
- \mathcal{C} flow set
- g jump map
- \mathcal{D} jump set

Hybrid dynamical systems

$$\begin{cases} \dot{x} = f(x), & x \in \mathcal{C}, \\ x^+ = g(x), & x \in \mathcal{D}. \end{cases}$$

Combine both worlds



Can model:

- Instantaneous events

$$x^+ = g(x), \quad x \in \mathcal{D}$$

- Discontinuous actions

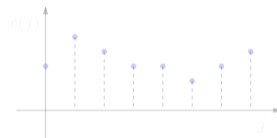
$q \in \{-1, 1\}$, q is a "logic" state variable

$$\dot{x} = f(x, q) = \begin{cases} f_+(x) & \text{if } q = 1, \\ f_-(x) & \text{if } q = -1. \end{cases}$$

Discrete-time systems

$$x^+ = g(x), \quad x \in \mathbb{R}^n$$

Model instantaneous events



Hybrid dynamical systems [Teel, Goebel, Sanfelice, 2012]: a tool for modeling discont. actions

Continuous-time systems

$$\dot{x} = f(x), \quad x \in \mathbb{R}^n$$

Model the dynamics of physical systems



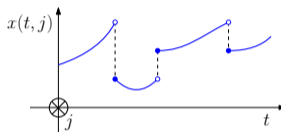
Terminology:

- f flow map
- \mathcal{C} flow set
- g jump map
- \mathcal{D} jump set

Hybrid dynamical systems

$$\begin{cases} \dot{x} = f(x), & x \in \mathcal{C}, \\ x^+ = g(x), & x \in \mathcal{D}. \end{cases}$$

Combine both worlds



Can model:

- Instantaneous events

$$x^+ = g(x), \quad x \in \mathcal{D}$$

- Discontinuous actions

$q \in \{-1, 1\}$, q is a "logic" state variable

$$\dot{x} = f(x, q) = \begin{cases} f_+(x) & \text{if } q = 1, \\ f_-(x) & \text{if } q = -1. \end{cases}$$

Discrete-time systems

$$x^+ = g(x), \quad x \in \mathbb{R}^n$$

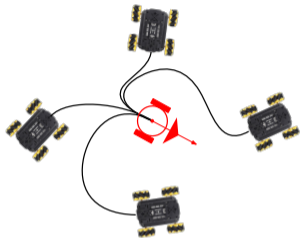
Model instantaneous events



**Design guidelines
(Hybrid Basic Conditions)**

- \mathcal{C}, \mathcal{D} closed
- f, g continuous

The HBC guarantees **robustness** of asymptotic stability to perturbations and uncertainties



- Goal: stabilize fw invariant compact set \mathcal{A}
- Given the equations of dynamics of vehicle

$$\dot{x} = f(x, u)$$

- Design hybrid control architecture s.t.

$$(\mathcal{H}) \begin{cases} \dot{x} = f(x, u), & x \in \mathcal{C}, \\ u = \kappa(x), & \\ x^+ = g(x), & x \in \mathcal{D}, \end{cases}$$

\mathcal{A} is GAS for (\mathcal{H})

Lyapunov-based control design methodology

- $u = \kappa(x), \mathcal{C}$
- $g(x), \mathcal{D}$
- $V(x)$ positive definite, radially unbounded

Choose

The control law driving the vehicle

The discontinuous action, when it happens

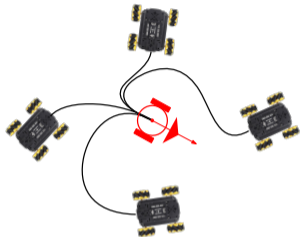
The Lyapunov function candidate

such that

$$\begin{aligned} \dot{V}(x) &= \nabla V(x)^\top f(x, \kappa(x)) < 0, & \forall x \in \mathcal{C} \setminus \mathcal{A} \\ \Delta V(x) &:= V(g(x)) - V(x) < 0, & \forall x \in \mathcal{D} \setminus \mathcal{A} \end{aligned}$$

V is decreasing along solutions to (\mathcal{H})

then, \mathcal{A} is Globally Asymptotically Stable (GAS)



- Goal: stabilize fw invariant compact set \mathcal{A}
- Given the equations of dynamics of vehicle

$$\dot{x} = f(x, u)$$

- Design hybrid control architecture s.t.

$$(\mathcal{H}) \begin{cases} \dot{x} = f(x, u), & x \in \mathcal{C}, \\ u = \kappa(x), & \\ x^+ = g(x), & x \in \mathcal{D}, \end{cases}$$

\mathcal{A} is GAS for (\mathcal{H})

Lyapunov-based control design methodology

- $u = \kappa(x), \mathcal{C}$
- $g(x), \mathcal{D}$
- $V(x)$ positive definite, radially unbounded

Choose

The control law driving the vehicle

The discontinuous action, when it happens

The Lyapunov function candidate

such that

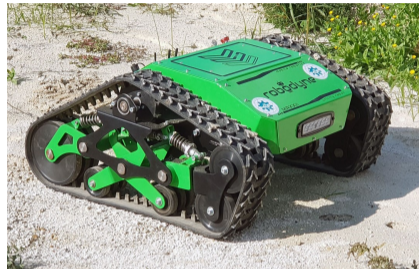
$$\begin{aligned} \dot{V}(x) &:= \nabla V(x)^\top f(x, \kappa(x)) \leq (?) 0, & \forall x \in \mathcal{C} \setminus \mathcal{A} \\ \Delta V(x) &:= V(g(x)) - V(x) \leq (?) 0, & \forall x \in \mathcal{D} \setminus \mathcal{A} \end{aligned}$$

V is **non-increasing (?)** along solutions to (\mathcal{H})

Behaviour of solutions can be exploited

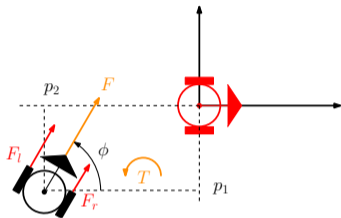
then, \mathcal{A} is Globally Asymptotically Stable (GAS)

- Introduction and background
 - Setting & Hybrid Systems & Lyapunov Stability
- Target stabilization
 - Unmanned Ground Vehicles (UGV)
- Recent Extensions
- Conclusions



Ballaben, R., Astolfi, A., Braun, P., & Zaccarian, L. (2026b). *Orchestrating on-board sensors for global hybrid robust stabilization of unicycles* [Automatica]. <https://hal.science/hal-05004452>

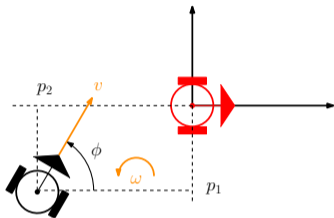
A kinematic model for UGV in the camera-based coordinates



Modeling assumptions

- F_r, F_l are independent
- F, T can be used to assign v, ω

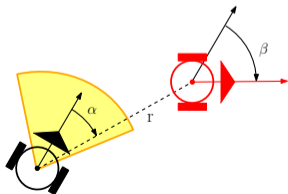
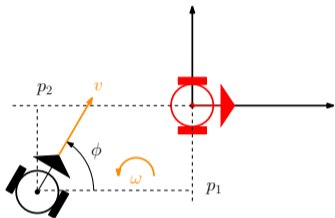
A kinematic model for UGV in the camera-based coordinates



Modeling assumptions

- F_r, F_l are independent
- F, T can be used to assign v, ω
- Under the modeling assumptions, the motion of a UGV is described by the kinematic equations

$$\begin{bmatrix} \dot{p}_1 \\ \dot{p}_2 \\ \dot{\phi} \end{bmatrix} = \begin{bmatrix} v \cos(\phi) \\ v \sin(\phi) \\ \omega \end{bmatrix},$$
$$u = [v \ \omega]^\top$$



Modeling assumptions

- F_r, F_l are independent
- F, T can be used to assign v, ω

- Under the modeling assumptions, the motion of a UGV is described by the kinematic equations

$$\begin{bmatrix} \dot{p}_1 \\ \dot{p}_2 \\ \dot{\phi} \end{bmatrix} = \begin{bmatrix} v \cos(\phi) \\ v \sin(\phi) \\ \omega \end{bmatrix},$$

$$u = [v \ \omega]^\top$$

- Exploiting the coordinate transformation $x = \gamma(z)$, the kinematic equations of a UGV in the camera-based coordinates are obtained

$$\begin{bmatrix} \dot{r} \\ \dot{\beta} \\ \dot{\alpha} \end{bmatrix} = \begin{bmatrix} -vr \cos(\alpha) \\ -\omega \\ v \sin(\alpha) - \omega \end{bmatrix},$$

$$\alpha \in [-\bar{\alpha}, \bar{\alpha}], \quad u = [v \ \omega] = \begin{bmatrix} \frac{v}{r} & \omega \end{bmatrix}^\top$$

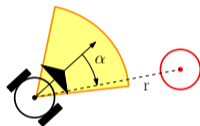
The measurements coming from one camera can be used to drive the vehicle to the target...

$$\star \dot{z} = \begin{bmatrix} \dot{r} \\ \dot{\beta} \\ \dot{\alpha} \end{bmatrix} = \begin{bmatrix} -\nu r \cos(\alpha) \\ -\omega \\ \nu \sin(\alpha) - \omega \end{bmatrix}, \quad \alpha \in [-\bar{\alpha}, \bar{\alpha}], \quad u = [\nu \ \omega] = \left[\frac{\nu}{r} \ \omega \right]$$

The measurements coming from one camera can be used to drive the vehicle to the target...

$$\star \dot{z} = \begin{bmatrix} \dot{r} \\ \dot{\beta} \\ \dot{\alpha} \end{bmatrix} = \begin{bmatrix} -\nu r \cos(\alpha) \\ -\omega \\ \nu \sin(\alpha) - \omega \end{bmatrix}, \quad \alpha \in [-\bar{\alpha}, \bar{\alpha}], \quad u = [\nu \ \omega] = \begin{bmatrix} \nu \\ \omega \end{bmatrix}$$

Camera measures (r, α)



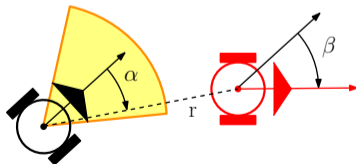
$$\kappa_0(r, \alpha) := \begin{bmatrix} k_r \cos(\alpha) \\ k_r \cos(\alpha) \sin(\alpha) + k_{\alpha} \alpha \end{bmatrix}$$

Theorem: Stabilization of target position

Let $k_r, k_{\alpha} \in \mathbb{R}_{>0}$ be arbitrary and $u = \kappa_0(r, \alpha)$. The set $\mathcal{A}_{\phi} = \{r = \alpha = 0\}$ is pre-asymptotically stable (pAS) for \star .

$$V(z) = \frac{1}{2}(r^2 + \alpha^2)$$

Camera measures $z = (r, \beta, \alpha)$



$$\kappa(z) = \begin{bmatrix} k_r \cos(\alpha) \\ k_r \cos(\alpha) \sin(\alpha) + k_{\alpha} \alpha + k_{\beta} (\alpha - \beta) \frac{\cos(\alpha) \sin(\alpha)}{\alpha} \end{bmatrix}$$

Theorem: Stabilization of the target pose

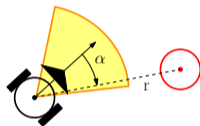
Let $k_r, k_{\beta}, k_{\alpha} \in \mathbb{R}_{>0}$ be arbitrary and $u = \kappa(z)$. The origin $\mathcal{A} = (0, 0, 0)$ is pAS for \star .

$$V(z) = \frac{1}{2} \left(r^2 + \frac{k_{\beta}}{k_r} (\alpha - \beta)^2 + \alpha^2 \right)$$

The measurements coming from one camera can be used to drive the vehicle to the target...

$$\star \dot{z} = \begin{bmatrix} \dot{r} \\ \dot{\beta} \\ \dot{\alpha} \end{bmatrix} = \begin{bmatrix} -\nu r \cos(\alpha) \\ -\omega \\ \nu \sin(\alpha) - \omega \end{bmatrix}, \quad \alpha \in [-\bar{\alpha}, \bar{\alpha}], \quad u = [\nu \ \omega] = \begin{bmatrix} \nu \\ \omega \end{bmatrix}$$

Camera measures (r, α)



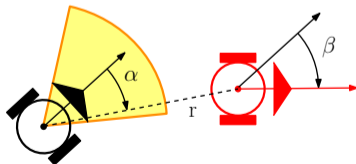
$$\kappa_0(r, \alpha) := \begin{bmatrix} k_r \cos(\alpha) \\ k_r \cos(\alpha) \sin(\alpha) + k_{\alpha} \alpha \end{bmatrix}$$

Theorem: Stabilization of target position

Let $k_r, k_{\alpha} \in \mathbb{R}_{>0}$ be arbitrary and $u = \kappa_0(r, \alpha)$. The set $\mathcal{A}_{\phi} = \{r = \alpha = 0\}$ is pre-asymptotically stable (pAS) for \star .

$$V(z) = \frac{1}{2}(r^2 + \alpha^2)$$

Camera measures $z = (r, \beta, \alpha)$



$$\kappa(z) = \begin{bmatrix} k_r \cos(\alpha) \\ k_r \cos(\alpha) \sin(\alpha) + k_{\alpha} \alpha + k_{\beta} (\alpha - \beta) \frac{\cos(\alpha) \sin(\alpha)}{\alpha} \end{bmatrix}$$

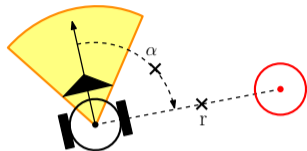
Theorem: Stabilization of the target pose

Let $k_r, k_{\beta}, k_{\alpha} \in \mathbb{R}_{>0}$ be arbitrary and $u = \kappa(z)$. The origin $\mathcal{A} = (0, 0, 0)$ is pAS for \star .

$$V(z) = \frac{1}{2} \left(r^2 + \frac{k_{\beta}}{k_r} (\alpha - \beta)^2 + \alpha^2 \right)$$

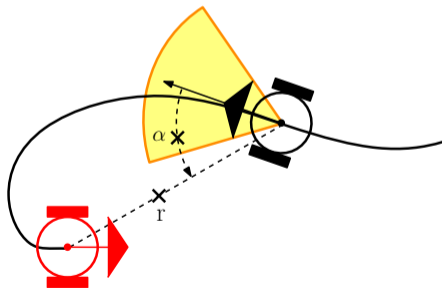
Solutions converge to the target if the target remains inside the field of view ($\alpha(t) \in [-\bar{\alpha}, \bar{\alpha}]$ for all t)

...but multiple cameras are required to achieve global stabilization



- The camera does not see the target for all possible configurations of the vehicle

$$\gamma(\mathcal{C} \cup \mathcal{D}) \neq \mathcal{X}$$



- The camera may lose vision of the target during the vehicle motion
- Not every solution to

$$\star \dot{z} = f(z, u) := \begin{bmatrix} \dot{r} \\ \dot{\beta} \\ \dot{\alpha} \end{bmatrix} = \begin{bmatrix} -\nu r \cos(\alpha) \\ -\omega \\ \nu \sin(\alpha) - \omega \end{bmatrix},$$

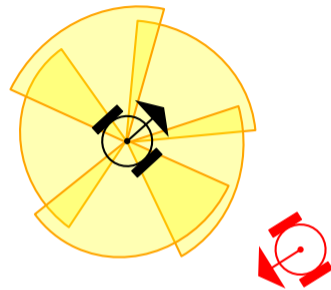
$$u = \kappa(z),$$

$$\alpha \in [-\bar{\alpha}, \bar{\alpha}]$$

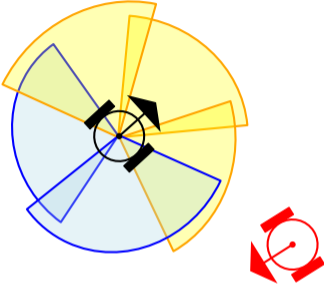
is complete ($t \mapsto z(t)$ defined $\forall t \geq 0$)

Measurements from multiple cameras must be combined to globally stabilize the target

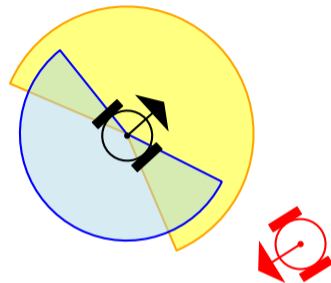
Multiple cameras can be combined into virtual front and rear camera, leading to forward and reverse motion



Multiple cameras can be combined into virtual front and rear camera, leading to forward and reverse motion



Multiple cameras can be combined into virtual front and rear camera, leading to forward and reverse motion

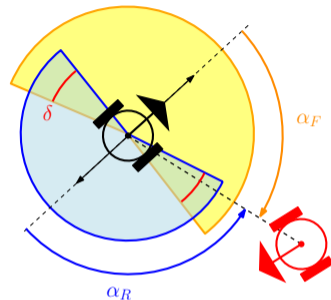


Multiple cameras can be combined into virtual front and rear camera, leading to forward and reverse motion

Two-cameras setup

Group cameras into a virtual **front** and **rear** camera

- **Front camera** measures (r, β, α_F) if $\alpha_F \in [-\frac{\pi}{2} - \delta, \frac{\pi}{2} + \delta]$
- **Rear camera** measures (r, β, α_R) if $\alpha_R \in [-\frac{\pi}{2} - \delta, \frac{\pi}{2} + \delta]$
- $\delta \in (0, \frac{\pi}{2})$ defines overlapping field of view of cameras



Multiple cameras can be combined into virtual front and rear camera, leading to forward and reverse motion

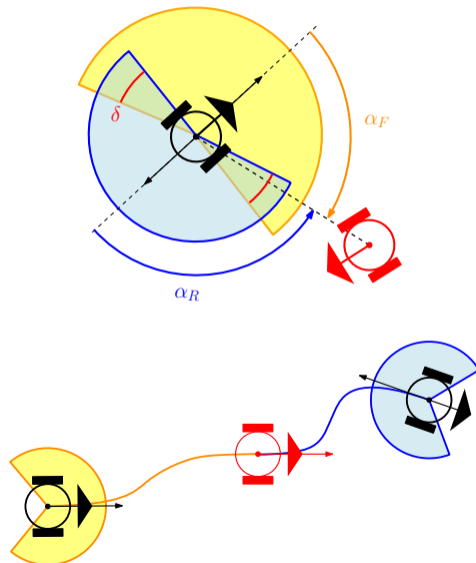
Two-cameras setup

Group cameras into a virtual **front** and **rear** camera

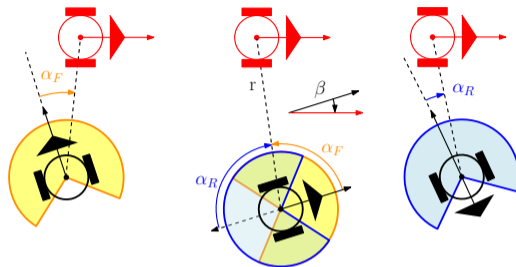
- **Front camera** measures (r, β, α_F) if $\alpha_F \in [-\frac{\pi}{2} - \delta, \frac{\pi}{2} + \delta]$
- **Rear camera** measures (r, β, α_R) if $\alpha_R \in [-\frac{\pi}{2} - \delta, \frac{\pi}{2} + \delta]$
- $\delta \in (0, \frac{\pi}{2})$ defines overlapping field of view of cameras

Discontinuous control action

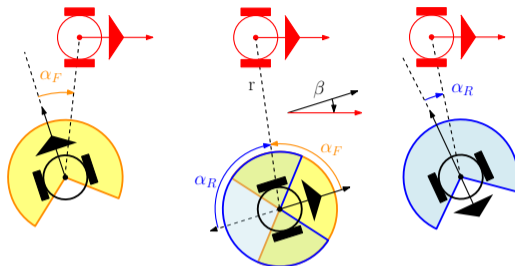
- **Front camera** sees the target $\Rightarrow \alpha_F \rightarrow 0 \Rightarrow$ **forward** motion ($v_1 > 0$)
- **Rear camera** sees the target $\Rightarrow \alpha_R \rightarrow 0 \Rightarrow$ **reverse** motion ($v_1 < 0$)



The target can be stabilized using front and rear camera measurements



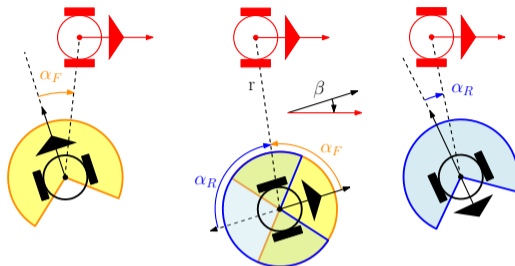
The target can be stabilized using front and rear camera measurements



- Two sets of coordinates $\mathbf{z}_F = (r, \beta, \alpha_F)$ and $\mathbf{z}_R = (r, \beta, \alpha_R)$

$$\alpha_i \in [-\frac{\pi}{2} - \delta, \frac{\pi}{2} + \delta], \quad i \in \{F, R\}, \quad \delta \in (0, \frac{\pi}{2})$$

The target can be stabilized using front and rear camera measurements



- Two sets of coordinates $\mathbf{z}_F = (r, \beta, \alpha_F)$ and $\mathbf{z}_R = (r, \beta, \alpha_R)$

$$\alpha_i \in [-\frac{\pi}{2} - \delta, \frac{\pi}{2} + \delta], \quad i \in \{F, R\}, \quad \delta \in (0, \frac{\pi}{2})$$

- Two sets of kinematic equations

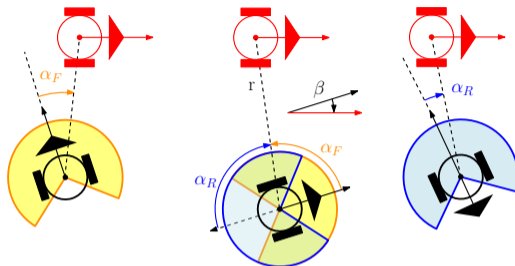
$$\star \dot{\mathbf{z}}_F = \begin{bmatrix} \dot{r} \\ \dot{\beta}_F \\ \dot{\alpha}_F \end{bmatrix} = \begin{bmatrix} -vr \cos(\alpha_F) \\ -\omega \\ +v \sin(\alpha_F) - \omega \end{bmatrix}$$

$$\alpha_F \in [-\frac{\pi}{2} - \delta, \frac{\pi}{2} + \delta]$$

$$\star \dot{\mathbf{z}}_R = \begin{bmatrix} \dot{r} \\ \dot{\beta}_R \\ \dot{\alpha}_R \end{bmatrix} = \begin{bmatrix} +vr \cos(\alpha_R) \\ -\omega \\ -v \sin(\alpha_R) - \omega \end{bmatrix}$$

$$\alpha_R \in [-\frac{\pi}{2} - \delta, \frac{\pi}{2} + \delta]$$

The target can be stabilized using front and rear camera measurements



- Two sets of coordinates $\mathbf{z}_F = (r, \beta, \alpha_F)$ and $\mathbf{z}_R = (r, \beta, \alpha_R)$

$$\alpha_i \in [-\frac{\pi}{2} - \delta, \frac{\pi}{2} + \delta], \quad i \in \{F, R\}, \quad \delta \in (0, \frac{\pi}{2})$$

- Two sets of kinematic equations

$$\star \dot{\mathbf{z}}_F = \begin{bmatrix} \dot{r} \\ \dot{\beta}_F \\ \dot{\alpha}_F \end{bmatrix} = \begin{bmatrix} -vr \cos(\alpha_F) \\ -\omega \\ +v \sin(\alpha_F) - \omega \end{bmatrix}$$

$$\alpha_F \in [-\frac{\pi}{2} - \delta, \frac{\pi}{2} + \delta]$$

$$\star \dot{\mathbf{z}}_R = \begin{bmatrix} \dot{r} \\ \dot{\beta}_R \\ \dot{\alpha}_R \end{bmatrix} = \begin{bmatrix} +vr \cos(\alpha_R) \\ -\omega \\ -v \sin(\alpha_R) - \omega \end{bmatrix}$$

$$\alpha_R \in [-\frac{\pi}{2} - \delta, \frac{\pi}{2} + \delta]$$

- Two stabilizers $i \in \{F, R\}$

Target position stabilizer

$$\kappa_0(\mathbf{z}_F/\mathbf{z}_R) = \begin{bmatrix} +/ - k_r \cos(\alpha_i) \\ k_r \cos(\alpha_i) \sin(\alpha_i) + k_\alpha \alpha_i \end{bmatrix}$$

Target pose stabilizer

$$\kappa(\mathbf{z}_F/\mathbf{z}_R) = \begin{bmatrix} +/ - k_r \cos(\alpha_i) \\ k_r \cos(\alpha_i) \sin(\alpha_i) + k_\alpha \alpha_i + k_\beta (\alpha_i - \beta) \frac{\cos(\alpha_i) \sin(\alpha_i)}{\alpha_i} \end{bmatrix}$$

A hybrid control architecture can combine front and rear camera measurements

- A logic variable $q \in \{-1, 1\}$ can be used to describe the camera used
- Hybrid state combines camera measurements with logic variable

$$\xi = (r, \beta, \alpha, q)$$

$$q = 1 \Rightarrow (r, \beta, \alpha) = z_F$$

$$q = -1 \Rightarrow (r, \beta, \alpha) = z_R$$

A hybrid control architecture can combine front and rear camera measurements

- A logic variable $q \in \{-1, 1\}$ can be used to describe the camera used
- Hybrid state combines camera measurements with logic variable

$$\xi = (r, \beta, \alpha, q)$$

$$q = 1 \Rightarrow (r, \beta, \alpha) = z_F$$

$$q = -1 \Rightarrow (r, \beta, \alpha) = z_R$$

- Logic variable q unifies equations of motion and feedback selections into **flow dynamics**

$$\dot{\xi} = \begin{bmatrix} \dot{r} \\ \dot{\beta} \\ \dot{\alpha} \\ \dot{q} \end{bmatrix} = f(\xi, u) := \begin{bmatrix} -q\nu r \cos(\alpha) \\ -\omega \\ q\nu \sin(\alpha) - \omega \\ 0 \end{bmatrix}, \quad \xi \in \mathcal{C}, \quad u = \kappa(\xi) = \begin{bmatrix} qk_r \cos(\alpha) \\ k_r \cos(\alpha) \sin(\alpha) + k_\alpha \alpha + k_\beta (\alpha - \beta) \frac{\cos(\alpha) \sin(\alpha)}{\alpha} \end{bmatrix},$$
$$\mathcal{C} = \{\xi : |\alpha| \leq \frac{\pi}{2} + \delta\}$$

A hybrid control architecture can combine front and rear camera measurements

- A logic variable $q \in \{-1, 1\}$ can be used to describe the camera used
- Hybrid state combines camera measurements with logic variable

$$\xi = (r, \beta, \alpha, q)$$

$$q = 1 \Rightarrow (r, \beta, \alpha) = z_F$$

$$q = -1 \Rightarrow (r, \beta, \alpha) = z_R$$

- Logic variable q unifies equations of motion and feedback selections into **flow dynamics**

$$\dot{\xi} = \begin{bmatrix} \dot{r} \\ \dot{\beta} \\ \dot{\alpha} \\ \dot{q} \end{bmatrix} = f(\xi, u) := \begin{bmatrix} -q\nu r \cos(\alpha) \\ -\omega \\ q\nu \sin(\alpha) - \omega \\ 0 \end{bmatrix}, \quad \xi \in \mathcal{C}, \quad u = \kappa(\xi) = \begin{bmatrix} qk_r \cos(\alpha) \\ k_r \cos(\alpha) \sin(\alpha) + k_\alpha \alpha + k_\beta (\alpha - \beta) \frac{\cos(\alpha) \sin(\alpha)}{\alpha} \end{bmatrix},$$

$$\mathcal{C} = \{\xi : |\alpha| \leq \frac{\pi}{2} + \delta\}$$

- **Jump dynamics** defines the switch between cameras (the discontinuous action)

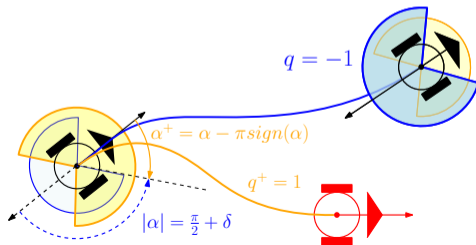
When cameras are switched

$$\xi \in \mathcal{D} := \{\xi : |\alpha| \geq \frac{\pi}{2} + \delta\}$$

How measurements change

$$\xi^+ = g(\xi) := \begin{bmatrix} r \\ \beta \\ \alpha - \pi \text{sign}(\alpha) \\ -q \end{bmatrix}$$

$\delta \in (0, \frac{\pi}{2})$ ensures **hysteresis** in the camera switch



Reset of vehicle orientation

- Hybrid state combines camera measurements with logic variable

$$\xi = (r, \beta, \alpha, q), \quad \alpha \in [-\frac{\pi}{2} - \delta, \frac{\pi}{2} + \delta], \quad \beta \in [-\frac{3}{2}\pi - \delta, \frac{3}{2}\pi + \delta]$$

$$q = 1 \Rightarrow (r, \beta, \alpha) = z_F \qquad q = -1 \Rightarrow (r, \beta, \alpha) = z_R$$

- Logic variable q unifies equations of motion and feedback selections into flow dynamics

$$\dot{\xi} = \begin{bmatrix} \dot{r} \\ \dot{\beta} \\ \dot{\alpha} \\ \dot{q} \end{bmatrix} = f(\xi, u) := \begin{bmatrix} -qv r \cos(\alpha) \\ -\omega \\ qv \sin(\alpha) - \omega \\ 0 \end{bmatrix}, \quad \xi \in \mathcal{C}, \quad u = \kappa(\xi) = \begin{bmatrix} qk_r \cos(\alpha) \\ k_r \cos(\alpha) \sin(\alpha) + k_\alpha \alpha + k_\beta (\alpha - \beta) \frac{\cos(\alpha) \sin(\alpha)}{\alpha} \end{bmatrix},$$

$$\mathcal{C} = \{\xi : |\alpha| \leq \frac{\pi}{2} + \delta, \beta \in [-\frac{3}{2}\pi - \delta, \frac{3}{2}\pi + \delta]\}$$

- Jump dynamics

Camera switch

$$\mathcal{D}_\alpha := \{\xi \in \Xi : |\alpha| \geq \frac{\pi}{2} + \delta\}$$

$$g_\alpha(\xi) := \begin{bmatrix} r \\ \beta \\ \alpha - \pi \text{sign}(\alpha) \\ -q \end{bmatrix}$$

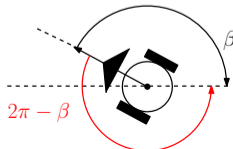
Orientation reset

$$\mathcal{D}_\beta := \{\xi \in \Xi : |\beta| \geq \frac{3}{2}\pi + \delta\}$$

$$g_\beta(\xi) := \begin{bmatrix} r \\ \beta - 2\pi \text{sign}(\beta) \\ \alpha \\ q \end{bmatrix}$$

$$\xi^+ \in G(\xi) = \begin{cases} \{g_\beta(\xi)\}, & \text{if } \xi \in \mathcal{D}_\beta \setminus \mathcal{D}_\alpha, \\ \{g_\alpha(\xi)\}, & \text{if } \xi \in \mathcal{D}_\alpha \setminus \mathcal{D}_\beta, \\ \{g_\alpha(\xi)\} \cup \{g_\beta(\xi)\}, & \text{if } \xi \in \mathcal{D}_\alpha \cap \mathcal{D}_\beta, \end{cases}$$

$$\mathcal{D} := \mathcal{D}_\alpha \cup \mathcal{D}_\beta$$



- Closed-loop hybrid system

$$(\mathcal{H}) \begin{cases} \dot{\xi} = f(\xi, \kappa(\xi)), & \xi \in \mathcal{C}, \\ \xi^+ \in g(\xi), & \xi \in \mathcal{D}. \end{cases}$$

- The Lyapunov function candidate

$$V(\xi) = \frac{1}{2} \left(r^2 + \frac{k_\beta}{k_r} (\alpha - \beta)^2 + \alpha^2 \right)$$

is non-increasing when solutions flow ($\dot{V} \leq 0$), but **may increase when solutions jump** from \mathcal{D}_α !

Main result: global stabilization of target using camera measurements

- Closed-loop hybrid system

$$(\mathcal{H}) \begin{cases} \dot{\xi} = f(\xi, \kappa(\xi)), & \xi \in \mathcal{C}, \\ \xi^+ \in g(\xi), & \xi \in \mathcal{D}. \end{cases}$$

- The Lyapunov function candidate

$$V(\xi) = \frac{1}{2} \left(r^2 + \frac{k_\beta}{k_r} (\alpha - \beta)^2 + \alpha^2 \right)$$

is non-increasing when solutions flow ($\dot{V} \leq 0$), but **may increase when solutions jump** from \mathcal{D}_α !

Lemma: camera invariance

All solutions to (\mathcal{H}) jump from \mathcal{D}_α at most once.

Theorem: Target stabilization via two-cameras architecture

For any selection of control gains $k_r, k_\alpha \in \mathbb{R}_{>0}$, $k_\beta \in \mathbb{R}_{\geq 0}$ and $\delta \in (0, \frac{\pi}{2})$

- $\mathcal{A}_\phi = \{r = \alpha = 0\}$ is GAS for (\mathcal{H})
- If $k_\beta > 0$, $\mathcal{A} = \{r = \alpha = \beta = 0\}$ is GAS for (\mathcal{H})
- All solutions are complete

Main result: global stabilization of target using camera measurements

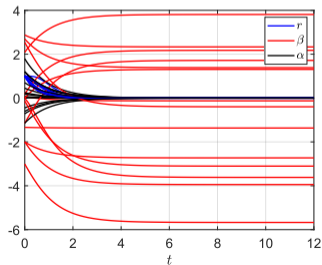
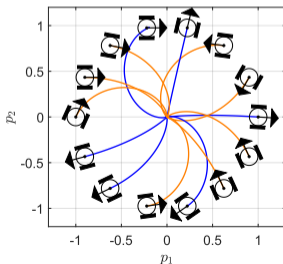
- Closed-loop hybrid system

$$(\mathcal{H}) \begin{cases} \dot{\xi} = f(\xi, \kappa(\xi)), & \xi \in \mathcal{C}, \\ \xi^+ \in g(\xi), & \xi \in \mathcal{D}. \end{cases}$$

- The Lyapunov function candidate

$$V(\xi) = \frac{1}{2} \left(r^2 + \frac{k_\beta}{k_r} (\alpha - \beta)^2 + \alpha^2 \right)$$

is non-increasing when solutions flow ($\dot{V} \leq 0$), but **may increase when solutions jump** from \mathcal{D}_α !



Lemma: camera invariance

All solutions to (\mathcal{H}) jump from \mathcal{D}_α at most once.

Theorem: Target stabilization via two-cameras architecture

For any selection of control gains $k_r, k_\alpha \in \mathbb{R}_{>0}$, $k_\beta \in \mathbb{R}_{\geq 0}$ and $\delta \in (0, \frac{\pi}{2})$

- $\mathcal{A}_\phi = \{r = \alpha = 0\}$ is GAS for (\mathcal{H})
- If $k_\beta > 0$, $\mathcal{A} = \{r = \alpha = \beta = 0\}$ is GAS for (\mathcal{H})
- All solutions are complete

Main result: global stabilization of target using camera measurements

- Closed-loop hybrid system

$$(\mathcal{H}) \begin{cases} \dot{\xi} = f(\xi, \kappa(\xi)), & \xi \in \mathcal{C}, \\ \xi^+ \in g(\xi), & \xi \in \mathcal{D}. \end{cases}$$

- The Lyapunov function candidate

$$V(\xi) = \frac{1}{2} \left(r^2 + \frac{k_\beta}{k_r} (\alpha - \beta)^2 + \alpha^2 \right)$$

is non-increasing when solutions flow ($\dot{V} \leq 0$), but **may increase when solutions jump** from \mathcal{D}_α !

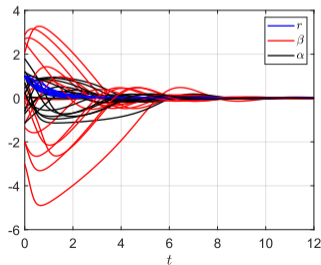
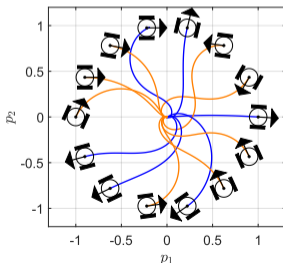
Lemma: camera invariance

All solutions to (\mathcal{H}) jump from \mathcal{D}_α at most once.

Theorem: Target stabilization via two-cameras architecture

For any selection of control gains $k_r, k_\alpha \in \mathbb{R}_{>0}$, $k_\beta \in \mathbb{R}_{\geq 0}$ and $\delta \in (0, \frac{\pi}{2})$

- $\mathcal{A}_\phi = \{r = \alpha = 0\}$ is GAS for (\mathcal{H})
- If $k_\beta > 0$, $\mathcal{A} = \{r = \alpha = \beta = 0\}$ is GAS for (\mathcal{H})
- All solutions are complete



$$(\mathcal{H}) \begin{cases} \dot{\xi} = f(\xi, \kappa(\xi)), & \xi \in \mathcal{C}, \\ \xi^+ \in g(\xi), & \xi \in \mathcal{D}. \end{cases}$$

(\mathcal{H}) satisfies the HBC

HBC guarantee robustness of GAS

Theorem: Robustness to perturbations, measurement noise, and switch uncertainties

There exists a non-trivial perturbation function $\xi \mapsto \mu(\xi)$ such that \mathcal{A} is GAS for the perturbed system (\mathcal{H}_μ)

$$(\mathcal{H}_\mu) \begin{cases} \dot{\xi} = f(\xi, \kappa(\xi)), & \xi \in \mathcal{C}, \\ \xi^+ \in g(\xi), & \xi \in \mathcal{D}. \end{cases}$$

Robustness of GAS is guaranteed by hybrid well-posedness

$$(\mathcal{H}) \begin{cases} \dot{\xi} = f(\xi, \kappa(\xi)), & \xi \in \mathcal{C}, \\ \xi^+ \in g(\xi), & \xi \in \mathcal{D}. \end{cases}$$

(\mathcal{H}) satisfies the HBC

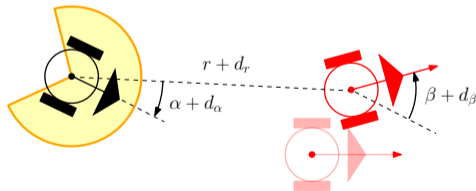
HBC guarantee robustness of GAS

Theorem: Robustness to perturbations, measurement noise, and switch uncertainties

There exists a non-trivial perturbation function $\xi \mapsto \mu(\xi)$ such that \mathcal{A} is GAS for the perturbed system (\mathcal{H}_μ)

$$(\mathcal{H}_\mu) \begin{cases} \dot{\xi} \in f(\xi, \kappa(\xi + \mu(\xi)\mathbb{B})), & \xi \in \mathcal{C}, \\ \xi^+ \in g(\xi), & \xi \in \mathcal{D}. \end{cases}$$

- Measurement errors in the feedback



Robustness of GAS is guaranteed by hybrid well-posedness

$$(\mathcal{H}) \begin{cases} \dot{\xi} = f(\xi, \kappa(\xi)), & \xi \in \mathcal{C}, \\ \xi^+ \in g(\xi), & \xi \in \mathcal{D}. \end{cases}$$

(\mathcal{H}) satisfies the HBC

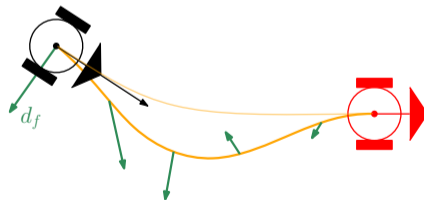
HBC guarantee robustness of GAS

Theorem: Robustness to perturbations, measurement noise, and switch uncertainties

There exists a non-trivial perturbation function $\xi \mapsto \mu(\xi)$ such that \mathcal{A} is GAS for the perturbed system (\mathcal{H}_μ)

$$(\mathcal{H}_\mu) \begin{cases} \dot{\xi} \in f(\xi, \kappa(\xi + \mu(\xi)\mathbb{B})) + \mu(\xi)\mathbb{B}, & \xi \in \mathcal{C}, \\ \xi^+ \in g(\xi) + \mu(\xi)\mathbb{B}, & \xi \in \mathcal{D}. \end{cases}$$

- Measurement errors in the feedback
- **Arbitrary external perturbations**



Robustness of GAS is guaranteed by hybrid well-posedness

$$(\mathcal{H}) \begin{cases} \dot{\xi} = f(\xi, \kappa(\xi)), & \xi \in \mathcal{C}, \\ \xi^+ \in g(\xi), & \xi \in \mathcal{D}. \end{cases}$$

(\mathcal{H}) satisfies the HBC

HBC guarantee robustness of GAS

Theorem: Robustness to perturbations, measurement noise, and switch uncertainties

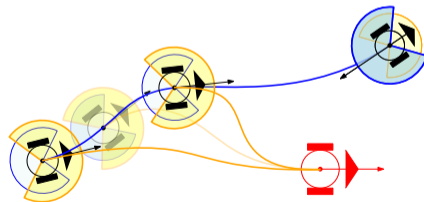
There exists a non-trivial perturbation function $\xi \mapsto \mu(\xi)$ such that \mathcal{A} is GAS for the perturbed system (\mathcal{H}_μ)

$$(\mathcal{H}_\mu) \begin{cases} \dot{\xi} \in f(\xi, \kappa(\xi + \mu(\xi)\mathbb{B})) + \mu(\xi)\mathbb{B}, & \xi \in \mathcal{C}_\mu, \\ \xi^+ \in g(\xi) + \mu(\xi)\mathbb{B}, & \xi \in \mathcal{D}_\mu. \end{cases}$$

- Measurement errors in the feedback
- Arbitrary external perturbations
- **Uncertainties affecting the switch time**

$$\mathcal{C}_\mu = \{\xi : |\alpha| \leq \frac{\pi}{2} + \delta + \mu(\xi)\},$$

$$\mathcal{D}_\mu = \{\xi : |\alpha| \leq \frac{\pi}{2} + \delta - \mu(\xi)\}.$$



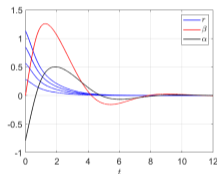
Stability properties in the Cartesian coordinates

AS in the polar coordinates $z = (r, \beta, \alpha) \Rightarrow ?$ AS in the Cartesian coordinates $x = (p_1, p_2, \phi)$

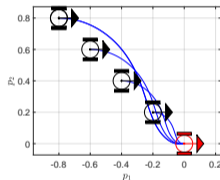
The Cartesian state x can be seen as an **output** of the system

$$\star \begin{cases} \dot{z} &= f(z, \kappa(z)) \\ x &= \gamma(z) \end{cases}$$

- $|x|^2 = p_1^2 + p_2^2 + \phi^2 \stackrel{x=\gamma(z)}{=} r^2 + \beta^2 \leq |z|^2$
 $\Rightarrow |z(t)| \rightarrow 0$ implies $|x(t)| \rightarrow 0 \Rightarrow$ **attractivity**

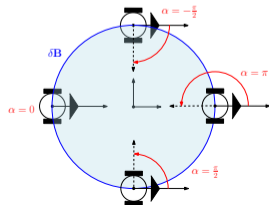


- $|x(0)| \leq \delta_x$ does **NOT** imply $|z(0)| \leq \delta_z!$
 \Rightarrow large $|z(0)|$ can lead to $\beta(t) = -\phi(t)$ overshoot!



- The coordinate transformation $x = \gamma(z)$ is not a **homeomorphism!**

$$(r, \beta, \alpha) = \gamma^{-1}(\delta\mathbb{B}) = [0, \delta] \times [0, \delta] \times (-\pi, \pi]$$



Stabilization in polar coordinates guarantees convergence in Cartesian coordinates

• Introduction and background

- Setting & Hybrid Systems & Lyapunov Stability

• Target stabilization

- Unmanned Ground Vehicles (UGV)

• Recent Extensions

- Unmanned Surface Vehicles (USV)



Ballaben, R., Astolfi, A., Braun, P., & Zaccarian, L. (2025). *Towards global stabilization of a hovercraft model using hybrid systems and discontinuous feedback laws* [CDC]. Ballaben, R., Astolfi, A., Braun, P., & Zaccarian, L. (2026a). *Hybrid orchestration of onboard cameras for global stabilization of a hovercraft* [Conditionally accepted: IFAC Nonlinear Analysis: Hybrid Systems].

